

ETRIS - Geo-INQUIRE online training course, First Day: November 6, 2023 Empirical fragility and vulnerability curves for risk analysis (VA2-35-1)

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Lecture by: Fatemeh Jalayer University College London (UCL)

Moderator: Hossein Ebrahimian University of Naples Federico II (UNINA)



UCL

University College London INSTITUTE FOR RISK AND DISASTER REDUCTION (IRDR)



European Tsunami Risk Service (ETRIS) Candidate Thematic Core Service (cTCS-Tsu)







Agenda: First Day, November 6th

- Introduction to Geo-INQUIRE
- Introduction to EPOS, Tsunami cTCS, and ETRiS
- The forward probabilistic framework
- Damage scales

- Definition of fragility function
- The fragility function for a class of assets
- The definition of vulnerability function
- Empirical fragility curves
- Empirical fragility assessment using GLM
- Bayesian model class selection
- Examples

Geo-INQUIRE Project (https://www.geo-inquire.eu/)

- **Geo-INQUIRE** will provide and enhance access to selected key data, products, and services, enabling the dynamic processes within the geosphere to be monitored and modelled at new levels of spatial and temporal detail and precision.
- **Geo-INQUIRE** benefits from a unique partnership of 51 partners consisting of major national research institutes, universities, national geological surveys, and European consortia.
- Geo-INQUIRE aims to enhance the scientific community's awareness of the available assets by carrying out dedicated training programs to ensure the optimal use of the services, to support access, and to liaise with scientific users to understand how to continuously adapt the services to meet their needs.

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European Plate Observing System (EPOS)



EPOS, the European Plate Observing System, is a multidisciplinary, distributed research infrastructure that facilitates the integrated use of data, data products, and facilities from the solid Earth science community in Europe.



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Candidate Thematic Core Service Tsunami (cTCS Tsunami)

cTCS Tsunami aims to establish sustainable and harmonized services for Tsunami Science and Tsunami Risk Reduction and to coordinate the provision of access to - and interaction with - data, products, software, workflows, and other services on a European level and beyond.

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Currently 30 partner institutions across Europe from 14 countries







The European Tsunami Risk Service (ETRiS)

The European Tsunami Risk Service (ETRiS) is a part of the cTCS Tsunami and is integrated into the data portal of EPOS. ETRiS aims to provide virtual access to Data, Data products, Software, and Services for tsunami vulnerability and risk components.

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What is the idea behind ETRiS?

- To provide researchers with tools that enable them to do research related to probabilistic tsunami risk assessment (PTRA).
- To post-process raw data in a harmonized way to produce data products.
- To provide open access also to the software used to post-process data.
- To provide access to data products that are useful for multi-hazard and multirisk applications.
- To provide training activities on how to use the codes to process data and how to use then for PTRA.

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A Forward Probabilistic Framework (PTRA)



Behrens, J., Løvholt, F., Jalayer, F., Lorito, S., Salgado-Gálvez, M.A., Sørensen, M., Abadie, S., Aguirre-Ayerbe, I., Aniel-Quiroga, I., Babeyko, A. and Baiguera, M., 2021. Probabilistic tsunami hazard and risk analysis: A review of research gaps. *Frontiers in Earth Science*, *9*, p.628772.

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Decision variable

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 The decision variable DV is the generic variable used to describe risk. It is by fact a "metric" of risk such as the number of fatalities, the total economic loss, the annual expected loss, etc.



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Exposed Asset

- The procedures we discuss today, apply in general to any asset exposed to risk, a building, a class of buildings, an infrastructure, a class of infrastructure.
- In certain cases, it can even apply to population at risk.
- Therefore, we use herein, the generic term "exposed asset" to refer to persons and things exposed to risk.





The intensity measure

• Tsunami intensity measure is a scalar or vector that plays the role of interface variable between hazard and vulnerability (e.g., wave amplitude, flow depth, current velocity, momentum flux, or maximum inundation height).



Tsunami Impact and Consequence Datasets

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- Euro-Mediterranean Tsunami Catalogue WFS (EMTC V2)
- Italian Tsunami Effects Database (ITED, <u>https://www.ics-c.epos-eu.org/</u>)
- Limited datasets in (csv format) are available on the site of ETRIS.

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Tsunami Impact and Consequence Datasets (continued)

- The Japanese Ministry of Land, Infrastructure, and Transport and Tourism (MLIT)
- https://www.mlit.go.jp/toshi/toshi-hukkou-arkaibu.html







Damage scale

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 Damage scale is the ensemble of *mutually exclusive ad* collectively exhaustive (MECE) damage states used to described the *whole* range of possibilities in terms of damage for an exposed asset.





Mutually Exclusive and Collectively Exhaustive Damage States

Damage states $\{DS_0, DS_1, ..., DS_{N_{DS}}\}$ are mutually exclusive and collectively exhaustive (MECE) if an only if

- $P(DS_i \cdot DS_j | IM) = 0$ (if $i \neq j, j = 0: N_{DS}$)
- $\sum_{j=0}^{N_{DS}} P(DS_j | IM) = 1;$

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Damage Levels and Damage States

Damage levels D_j are the thresholds that separate the different MECE damage states DS_j .

$$DS_{j} \equiv (D \ge D_{j}) \cdot (D < D_{j+1})$$







Damage Scales: examples

Damage Level		Damage level description	-			
D ₀	None	no damage				
D	Light	non-structural damage				
D ₂	Minor	significant non-structural damage, minor structural damage		Damage Level		Damage level description
D_3	Moderate	significant structural and non-structural		D ₀	None	no damage
Ŭ		damage		D ₁	Repairable	Partial damage, repairable
D ₄	Severe	irreparable structural damage, will require demolition	\rightarrow	D ₂	Unrepairable	Partial damage, unrepairable
D ₅	Collapse	complete structural collapse	←→	D ₃	Complete	Complete structural collapse
		South Pacific 2009 Reese et al. 2011				Sulawesi 2018 Paulik et al. 2019

Reese, S., Bradley, B. A., Bind, J., Smart, G., Power, W., & Sturman, J. (2011). Empirical building fragilities from observed damage in the 2009 South Pacific tsunami. *Earth-Science Reviews*, *107*(1-2), 156-173.

Paulik, R., Gusman, A., Williams, J. H., Pratama, G. M., Lin, S. L., Prawirabhakti, A., ... & Suwarni, N. W. I. (2019). Tsunami hazard and built environment damage observations from Palu City after the September 28 2018 Sulawesi earthquake and tsunami. *Pure and Applied Geophysics*, *176*(8), 3305-3321.

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• This page provides access to tsunami vulnerability and risk data products. These data products include various PTRA components such as damage scales, fragility curves, consequence functions, and vulnerability curves. The taxonomy used for labelling elements exposed to risk is GED4ALL.

https://eurotsunamirisk.org/dataproducts/

• Examples of Damage Scales in Literature

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The definition of the fragility

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 In the context of risk assessment at at regional level, the fragility curve is defined as the probability of exceeding a specific damage level as a function of the intensity measure.

$$P(D > D_i | IM = im)$$





The (alternative) definition of the fragility

 The fragility curve can also be defined as the cumulative distribution function (CDF) of the intensity measure value corresponding to the threshold of the damage level:

$P(D > D_i | IM = im) = P(IM^{D_i} \le im) = F_{IM^{D_i}}(im)$

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The underlying assumptions

There are some implicit assumptions in the definition of fragility:

- The fragility function is a filter function applied to a homogenous Poisson Process to filter a certain type of event (e.g., those earthquakes which lead to exceeding a certain damage level, or those tsunami events which lead to exceeding a certain damage level).
- It is meaningful for a single system. It is assumed that with each new event of interest (from the "mother" Poisson Process), the system will be "renewed" back to its intact state (D₀).





Question: How can we define the concept of fragility for a building class?





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The concept of fragility curve for a class

- The fragility curve for a class can be derived by assuming that the portfolio of buildings in a class is replaced by an "average" representative building.
- The dispersion in the class fragility curve, in theory, should consider both the (1) variability in the different types of events (e.g., tsunamis, earthquakes) given the intensity measure; (2) the building-to-building variability within the class.



Empirical Fragility

- Empirical fragility curves are models derived from pairs of observed damage and intensity data for buildings and infrastructure, usually collected, acquired and even partially simulated in the aftermath of disastrous events.
- This implies that damage data are obtained for a group of spatiallydistributed surveyed exposed assets.



The empirical fragility curves for a class

 The fragility curve for a class can be derived by assuming that the portfolio of surveyed buildings represent a "class" or are subdivided into more classes and that each class is replaced by an "average" representative structural model.

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The empirical fragility curves for a class

- This implies a sort of "spatial ergodicity"; that is, the surveyed damage data can be considered as different realizations of the average structural model to the event of interest.
- One consequence of such assumption is that the building-to-building variability is going to be considered in "disguise" and as a contribution to fragility curve dispersion.

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The median intensity, η_{IM_c} , for a given damage level, is calculated as the *IM* corresponding to 50% probability on the fragility curve.





Equivalent Lognormal Statistics for Fragility Curve

• The logarithmic standard deviation (dispersion) of the equivalent lognormal fragility curve, β_{IM_c} , is estimated as as $\beta_{IM_c} = 0.50 \times \ln(IM_c^{84}/IM_c^{16})$.





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Equivalent Lognormal Statistics for Fragility Curve

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 β_{IIF} can be estimated as half of the (natural) logarithmic distance (along the *IM* axis) between the median intensities (i.e., 50% probability) of the fragility curves derived with 16% (denoted as IM^{84}) and 84% (IM^{16}) confidence levels, respectively; i.e., $\beta_{UF} =$ $0.50 \times \ln(IM^{84}/IM^{16})$.





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The Empirical Tsunami Risk Products – Fragility Layer

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Geo-localization of Class Fragility Data

- Considering the definition of the class fragility curves, it is important to note that the geo-localization of such data is usually not accurate because these curves (by definition) represent a portfolio of spatially distributed assets.
- The geo-localization, if possible, is indicative of the geographic area where the surveyed assets are located.





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The procedure for obtaining the empirical fragility curves

- Establish the class or classes of asset for which the fragility curves are to be obtained.
- Establish a spatial extent for gathering the empirical data. This extent should be large enough to represent the class(es) of interest and the range of damage states/levels data gathered for this class.
- Very important: Establish the "base domain". This essentially delineates the entire portfolio of assets being surveyed for damage.



The procedure for obtaining the empirical fragility curves (continued)

• Obtain the empirical damage data:

- By performing field surveys.
- Through remote sensing data (e.g., EMS-Copernicus Damage Grading Maps).
- Through machine-learning and AI.
- By using existing damage data from literature.

• For example, damage data from <u>Southeast Pacific Tsunami</u> Event

Reese, Stefan, Brendon A. Bradley, Jochen Bind, Graeme Smart, William Power, and James Sturman. "Empirical building fragilities from observed damage in the 2009 South Pacific tsunami." *Earth-Science Reviews* 107, no. 1-2 (2011): 156-173.

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Damage data from Copernicus Grading Map

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Copernicus EMSR317 Palu Grading Map



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The procedure for obtaining the empirical fragility curves (continued)

- Obtain the intensity values at points of interest:
 - By performing field surveys and measurements
 - By spatial averaging (smoothing) of the field surveys and measurements
 - Through numerical simulation



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The different types of survey data

- **Aggregated**: where the IM information is reported as bins. In this case, the damage data will report the number of exposed asset in that IM bin that exceed a certain damage level (example, MLIT).
- **Point-wise**: In this case the IM values are reported at the position of each building (example Reese et al. 2011).
- The generalized regression routine presented here is applicable to both types of survey data.



The probability of being in a damage state DS given IM

• $P(D \ge D_j | IM)$ is the fragility function for damage level D_j .

$$\begin{split} P\left(DS_{j}\left|IM\right.\right) &= P\left[\left(D \ge D_{j}\right) \cdot \left(D < D_{j+1}\right)\right|IM\right] \\ &= \begin{cases} P\left(D \ge D_{j}\left|IM\right.\right) - P\left(D \ge D_{j+1}\left|IM\right.\right) & \text{for } 0 \le j < N_{DS} \\ P\left(D \ge D_{j}\left|IM\right.\right) & \text{for } j = N_{DS} \end{cases} \end{split}$$

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The representation of the fragility curve as P(DS|IM)

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 The probability mass function definition is used for providing the probability of a discrete variable; e.g., being in a given damage state DS.

$$P(DS_{j}|IM = im) = P(D > D_{j+1}|IM = im)$$

$$P(DS_{N_{DS}}|IM = im) = P(D > D_{N_{DS}}|IM = im)$$

$$\frac{DS_{0}}{D_{1}} \frac{DS_{1}}{D_{2}} \frac{DS_{2}}{D_{3}} \frac{DS_{3}}{D_{4}} \cdots \frac{DS_{N_{DS}}}{D_{N_{DS}}} DM$$



The Consequence Curve: Definition $G_{DV|DS}(dv | DS)$

 The consequence function can be formally defined as the probability distribution for the decision variable DV for (or conditioned on) a given damage state DS.



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G(dv|DS_i) = P(DV > dv|DS_i)f(DV = dv|DS = DS_i) = \left|\frac{dG(dv|DS_i)}{d \, dv}\right|
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Dan	nage_fac	tor	0	0.01	0.1	0.35	0.75	1	function (ma			
Dama Level	ge	Damage lev	vel des	cription					k	bui	ilding	s)
DS ₀	None	no damage										
DS ₁	Minor	Negligible structural da damage)	to sli mage;	ght dam slight non	age (no -structural	Hair-line crack Fall of small pi Fall of loose parts of building	s in very fe eces of plas stones fror gs in ver <u>y fe</u> v	ew walls. ster only. m upper w cases.	•			
DS ₂	Moderate	Moderate damage (slight structural Cracks in many walls. Fall of fairly damage; moderate non-structural large pieces of plaster. Partial damage) collapse of chimneys.							Damage k			
DS ₃	Major					Large and exte	nsive cracks	<mark>s in most</mark>	\sim	Lev	el	Damagene
		Substantial	to	heavy	damage	walls. Roof tile	s detach. C	Chimneys		D ₀	None	no damage
		(moderate s	structur	al damag	je; heavy	tracture at the	root line; t	allure of		D 1	Repairable	Partial dam
		non-structure	ai uama	ige)		(partitions; gab	e walls).	elements		D ₂	Unrepairable	Partial dam
DS ₄	Severe	Very heavy damage; ve damage)	damag ery he	le (heavy avy non-	structural -structural	Serious failure structural failur	of walls; par e of roofs ar	rtial nd		D ₃	Complete	Complete s
DS ₅	Collapse	Destruction	(very	heavy	structural	Total or near to	otal collapse.					Sulawesi 2 Paulik et a
		EMS 98 Da	mage \$	Scale Mas	onry				Pas New Italy	quale, / devel /. <i>Bulle</i>	G.D., Orsini, G. a opments in seism <i>tin of Earthquake</i>	nd Romeo, R.\ iic risk assessr <i>Engineering</i> , :

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	Dan Leve	nage el	Damage level description				
	D ₀	None	no damage				
Y	D ₁	Repairable	Partial damage, repairable				
	D ₂	Unrepairable	Partial damage, unrepairable				
~	D ₃	Complete	Complete structural collapse				
			Sulawesi 2018 Paulik et al. 2019				

W., 2005. ment in 3(1), pp.101-







The consequence function (masonry buildings)

Dan Lev	nage el	Damage level description		
D ₀	None	no damage		
\mathbf{D}_1	Repairable	Partial damage, repairable		
D ₂	Unrepairable	Partial damage, unrepairable		
D ₃	Complete	Complete structural collapse		
		Sulawesi 2018 Paulik et al. 2019		



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The consequence function (timber buildings)

• Tsunami Damage ratios from Goda et al. (2021) based on MLIT damage scale: DS_0 (0-0.03), $DS_1(0.03-0.1, 0.1-0.3)$, $DS_2(0.3-0.5, 0.5-1.0)$, and $DS_3(1.0)$, respectively for prevalently timber buildings.

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Goda, K., De Risi, R., De Luca, F., Muhammad, A., Yasuda, T., & Mori, N. (2021). Multi-hazard earthquake-tsunami loss estimation of Kuroshio Town, Kochi Prefecture, Japan considering the Nankai-Tonankai megathrust rupture scenarios. *International Journal of Disaster Risk Reduction*, *54*, 102050.





Data Products for Tsunami Risk Assessment

• <u>https://eurotsunamirisk.org/dataproducts/</u>

Some Examples of Consequence Functions in the Literature

Note that the consequence functions are not always formally defined as such, they can also be called cost model or the cost function.







Definition of the Vulnerability Curve

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• The vulnerability curve can be defined as the probability of distribution for the decision variable DV given the intensity measure IM.

$$G_{DV|IM}(dv|im) = P(DV > dv|IM = im)$$

$$G_{DV|IM}(dv|im) = \sum_{j=0}^{N_{DS}} G_{DV|DS_j}(dv|DS_j)P(DS_j|IM = im)$$

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Vulnerability curves



$$DS_0 DS_1 DS_2 DS_3 DS_3 DS_1 DS_{N_{DS}} DS_{N_{DS}} DS_{N_{DS}} DS_{N_{DS}} DM$$

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Definition of the Vulnerability Curve

 It is common to plot the vulnerability curve as the expected value (or median) and standard deviation of the decision variable DV (e.g., loss, fatalities) as a function of the intensity measure IM.

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The **Empirical** Tsunami **Risk Products** – **Vulnerability** Layer

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Using generalized regression for empirical fragility assessment



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The Bernoulli Variable Y

- For damage level D_j , all exposed asset with an observed damage level $D < D_j$ will have a probability equal to zero, while those with $D \ge D_j$ will have an assigned probability equal to one. In other words, for asset *i* and damage state *j*, the Bernoulli variable Y_{ij} indicates whether asset *i* is in damage state *j*:
 - $Y_{ij} = \begin{cases} 1 & \text{if asset } i \text{ exceeds } D_j & \text{with probability } P(D \ge D_j \mid IM_i) \\ 0 & \text{if asset } i \text{ does not exceed } D_j & \text{with probability } 1 P(D < D_j \mid IM_i) \end{cases}$

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Visualisation: The Bernoulli Variable Y

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Fragility Assessment for Hierarchical Damage Levels

• According to this method, fragility assessment is going to be performed for all the damage states as an ensemble.

$$P(DS_{j}|IM_{i}) = P[(D < D_{j+1}) \cdot (D \ge D_{j})|IM_{i}]$$

$$= [1 - P(D \ge D_{j+1}|D \ge D_{j}, IM_{i})] \cdot P(D \ge D_{j}|IM_{i})$$
Conditional Fragility
$$DS_{0} \quad DS_{1} \quad DS_{2} \quad DS_{3} \quad OB_{1} \quad DS_{2} \quad DS_{3} \quad OB_{N_{DS}} \quad DM$$

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Fragility Assessment using Generalized Regression

• Definition of viable fragility models:

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$$l_{ij} = \alpha_{0,j} + \alpha_{1,j} \ln IM_i$$

$$\pi_{ij} = \pi_j (IM_i) = \begin{cases} \left(1 + \exp(-l_{ij})\right)^{-1} & \log i \\ \Phi(l_{ij}) & \text{probit} \\ 1 - \exp(-\exp(l_{ij})) & \log \log \end{cases} \quad \mathbb{M}_2 \quad P(DS_j | IM_i) = \begin{bmatrix} 1 - \pi_{ij} \end{bmatrix} \quad P(D \ge D_j | IM_i)$$





Fragility Assessment using Generalized Regression

• The probabilities of being in different damage states can be calculated in a recursive way:

$$P(DS_{j}|IM_{i}) = \begin{cases} \left(1 - \pi_{ij}\right) \cdot \left[1 - \sum_{k=0}^{j-1} P(DS_{k}|IM_{i})\right] & \text{for } j \ge 1\\ 1 - \pi_{i0} \triangleq P(D < D_{1}|IM_{i}) & \text{for } j = 0 \end{cases}$$

$$P(DS_{N_{DS}} | IM_{i}) = P(D \ge D_{N_{DS}} | IM_{i}) = 1 - \sum_{j=0}^{N_{DS}-1} P(DS_{j} | IM_{i})$$
$$P(D \ge D_{j} | IM_{i}) = P(DS_{j} | IM_{i}) + P(D \ge D_{j+1} | IM_{i}) \quad \text{for } 0 \le j < N_{DS}$$

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Data for the point-wise case

- Data is defined as couples of (*IM*_i, *D*_i) obtained at the position i of each asset at risk.
- Position i can be defined by latitude and longitude of the point.
- $n_{CL,i}$ is the number of assets from typology *CL* in damage state DS_i
- Where *i* is going to vary from 1 to the number of buildings n_{CL,i}
- $D_{\rm i}$ can have values equal to $D_{\rm 0}$ to $D_{\rm NDS}$

$$DS_0 DS_1 DS_2 DS_3 DS_3 DS_{N_{DS}}$$

$$D_0 D_1 D_2 D_3 D_4 D_{N_{DS}} DM$$

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What if data for all damage states are not available?

 Let *index* be the vector of values indicating damage levels for which observed data are available. The new damage scale formed as

 $\{DS_{index(1)}, DS_{index(2)}, ..., DS_{index(N)}\}$, where *N* is the length of vector *index*, is also MECE.





Likelihood Calculation

• The likelihood is calculated as the probability of observing:

$$p(\mathbf{D} | \mathbf{\theta}_k, \mathbb{M}_k) = \prod_{j=0}^{N_{DS}} \prod_{i=1}^{n_{CL,j}} P(DS_j | IM_i)$$

• The vector of fragility model parameters θ_k

•
$$\theta = \left[\alpha_{0,1}, \alpha_{1,1}, \alpha_{0,2}, \alpha_{1,2,\dots,\alpha_{0,N_{DS-1}},\alpha_{1,N_{DS-1}}} \right]$$

• M_k is Model *k*, e.g., *k*=1:3



Likelihood Calculation for more than one class

• The likelihood is calculated as the probability of observing:

$$p(D|\theta_k, M_k) = \prod_{l=1}^{N_{CL}} \prod_{j=0}^{N_{DS}} \prod_{i=1}^{n_{CL_l, j}} P(DS_j | IM_i, CL_l)$$

• M_k is Model *k*, e.g., *k*=1:3

- \circ N_{CL} is the number of building classes
- $n_{CL_{l},j}$ is the number of assets from typology CL_{l} in damage state DS_{j}
- The vector of fragility model parameters θ_k

$$\circ \quad \theta_{k} = \left[\alpha_{0,1}, \alpha_{1,1}, \alpha_{0,2}, \alpha_{1,2,\dots,\alpha_{0,N_{DS-1}},\alpha_{1,N_{DS-1}}} \right]$$



The maximum likelihood estimation method

- A generalized linear regression model is used for the conditional fragility term $\pi_{ij} = P(D \ge D_{j+1} | D \ge D_j, IM)$ for the *j*th damage state DS_j , $0 \le j < N_{DS}$.
- Herein, we need to work with partial damage data so that all assets in DS_j (with an observed damage $D_j \le D < D_{j+1}$) will be assigned a probability equal to zero, while those in higher damage states (with $D \ge D_{j+1}$) will be assigned a probability equal to one (i.e., to model the conditioning on $D \ge D_j$, the domain of possible damage levels is reduced to $D \ge D_j$).



Bayesian model class selection (BMCS)

- We use the Bayesian model class selection (BMCS) to identify the best link model to use in the generalized linear regression scheme.
- However, the procedure is general and can be applied to a more diverse pool of candidate fragility models.
- BMCS (or model comparison) is essentially Bayesian updating at the model class level to make comparisons among candidate model classes given the observed data



Bayesian Model Class Selection

Given a set of N_M candidate model classes {M_k, k = 1: N_M}, and in the presence of the data **D**, the posterior probability of the kth model class, denoted as P(M_k|**D**) can be written as follows:

$$P(\mathbf{M}_{k}|\mathbf{D}) = \frac{p(\mathbf{D}|\mathbf{M}_{k})P(\mathbf{M}_{k})}{\sum_{k=1}^{N_{\mathbf{M}}} p(\mathbf{D}|\mathbf{M}_{k})P(\mathbf{M}_{k})}$$



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Bayesian Model Class Selection

• Let us define the vector of model parameters $\boldsymbol{\theta}_k$ for model class $\mathbb{M}_k \text{ as } \boldsymbol{\theta}_k = \left[\left\{ \alpha_{0,j}, \alpha_{1,j} \right\}_k, j = 0; N_{DS} - 1 \right]$. We use the Bayes theorem to write the "evidence" $p(\mathbf{D}|\mathbb{M}_k)$ provided by data **D** for model \mathbb{M}_k as follows:

$$p(\mathbf{D}|\mathbf{M}_{k}) = \frac{p(\mathbf{D}|\mathbf{\theta}_{k}, \mathbf{M}_{k}) p(\mathbf{\theta}_{k}|\mathbf{M}_{k})}{p(\mathbf{\theta}_{k}|\mathbf{D}, \mathbf{M}_{k})}$$

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The (log) evidence

that logarithm of the evidence (called *log-evidence*) ln[p(**D**|M_k)] can be written as:

$$\ln\left[p\left(\mathbf{D}|\mathbf{M}_{k}\right)\right] = \underbrace{\int_{\Omega_{\theta_{k}}} \ln\left[p\left(\mathbf{D}|\boldsymbol{\theta}_{k},\mathbf{M}_{k}\right)\right] p\left(\boldsymbol{\theta}_{k}|\mathbf{D},\mathbf{M}_{k}\right) d\boldsymbol{\theta}_{k}}_{Term 1} - \underbrace{\int_{\Omega_{\theta_{k}}} \ln\left[\frac{p\left(\boldsymbol{\theta}_{k}|\mathbf{D},\mathbf{M}_{k}\right)}{p\left(\boldsymbol{\theta}_{k}|\mathbf{M}_{k}\right)}\right] p\left(\boldsymbol{\theta}_{k}|\mathbf{D},\mathbf{M}_{k}\right) d\boldsymbol{\theta}_{k}}_{Term 2}$$

"Term 1" denotes the posterior mean of the log-likelihood, which is a measure of the average data fit to model M_k."Term 2" is the relative entropy between the prior p(θ_k|M_k) and the posterior p(θ_k|D, M_k) of θ_k given model M_k, which is a measure of the distance between the two PDFs.



The Posterior Distribution for Fragility Model Parameters

• The posterior distribution $p(\mathbf{\theta}_k | \mathbf{D}, \mathbf{M}_k)$ can be found based on Bayesian inference:

$$\underbrace{p(\mathbf{\theta}_{k} | \mathbf{D}, \mathbb{M}_{k})}_{\text{posterior}} = \frac{p(\mathbf{D} | \mathbf{\theta}_{k}, \mathbb{M}_{k}) p(\mathbf{\theta}_{k} | \mathbb{M}_{k})}{\int_{\Omega_{\mathbf{\theta}_{k}}} p(\mathbf{D} | \mathbf{\theta}_{k}, \mathbb{M}_{k}) p(\mathbf{\theta}_{k} | \mathbb{M}_{k}) d\mathbf{\theta}_{k}} = C^{-1} \underbrace{p(\mathbf{D} | \mathbf{\theta}_{k}, \mathbb{M}_{k})}_{\text{likelihood}} \underbrace{p(\mathbf{\theta}_{k} | \mathbb{M}_{k})}_{\text{prior}}$$

where C^{-1} is a normalizing constant.

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Markov Chain Monte Carlo Simulation Routine

- The prior distribution, p(θ_k|M_k), can be estimated as the product of marginal normal PDFs for each model parameter, i.e., a multivariate normal distribution with zero correlation between the pairs of model parameters θ_k.
- To sample from the posterior distribution $p(\theta_k | \mathbf{D}, \mathbf{M}_k)$, an *adaptive* MCMC simulation routine is employed.



Markov Chain Monte Carlo Simulation Routine (continued)

- MCMC is particularly useful for drawing samples from the target posterior, while it is known up to a scaling constant C^{-1} .
- Thus, we only need un-normalized PDFs to feed the MCMC procedure. The MCMC routine herein employs the Metropolis-Hastings (MH) algorithm to generate samples from the target joint posterior PDF.



Robust Fragility Assessment

 Robust Fragility (RF) is defined as the expected value for a prescribed fragility model considering the joint probability distribution for the fragility model parameters θ_k. The RF herein can be expressed as:

$$P\left(D \ge D_{j} | IM, \mathbf{D}, \mathbb{M}_{k}\right) = \int_{\Omega_{\boldsymbol{\theta}_{k}}} P\left(D \ge D_{j} | IM, \boldsymbol{\theta}_{k}\right) P\left(\boldsymbol{\theta}_{k} | \mathbf{D}, \mathbb{M}_{k}\right) d\boldsymbol{\theta}_{k} = \mathbb{E}_{\boldsymbol{\theta}_{k} | \mathbf{D}, \mathbb{M}_{k}} \left[P\left(D \ge D_{j} | IM, \boldsymbol{\theta}_{k}\right) \right]$$

$$\sigma_{\boldsymbol{\theta}_{k}|\mathbf{D},\mathbb{M}_{k}}^{2}\left[P\left(D \geq D_{j}\left|IM,\boldsymbol{\theta}_{k}\right.\right)\right] = \underbrace{\mathbb{E}_{\boldsymbol{\theta}_{k}|\mathbf{D},\mathbb{M}_{k}}\left[P\left(D \geq D_{j}\left|IM,\boldsymbol{\theta}_{k}\right.\right)^{2}\right]}_{\cong \frac{1}{N_{d}}\sum_{i=1}^{N_{d}}P\left(D \geq D_{j}\left|IM,\boldsymbol{\theta}_{k,i}\right.\right)^{2}} - \underbrace{\left(\mathbb{E}_{\boldsymbol{\theta}_{k}|\mathbf{D},\mathbb{M}_{k}}\left[P\left(D \geq D_{j}\left|IM,\boldsymbol{\theta}_{k}\right.\right)\right]\right)^{2}}_{=P\left(D \geq D_{j}\left|IM,\mathbf{D},\mathbb{M}_{k}\right.\right)^{2} \text{ (Eq.16)}}$$

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Using Monte Carlo Simulation for Fragility Assessment

• The RF integral can be solved numerically by employing Monte Carlo simulation with N_d generated samples from the vector $\boldsymbol{\theta}_k$ as follows:

$$P(D \ge D_j | IM, \mathbf{D}, \mathbb{M}_k) \cong \frac{1}{N_d} \sum_{l=1}^{N_d} P(D \ge D_j | IM, \mathbf{\theta}_{k,l})$$

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Using Monte Carlo Simulation for Fragility Assessment

 The integral equation for standard deviation of the fragility can be solved numerically by employing Monte Carlo simulation with N_d generated samples from the vector θ_k as follows:

$$\sigma_{\boldsymbol{\theta}_{k}|\mathbf{D},\mathbb{M}_{k}}^{2}\left[P\left(D \geq D_{j} \left| IM,\boldsymbol{\theta}_{k}\right.\right)\right] \cong \frac{1}{N_{d}} \sum_{i=1}^{N_{d}} P\left(D \geq D_{j} \left| IM,\boldsymbol{\theta}_{k,i}\right.\right)^{2} - P\left(D \geq D_{j} \left| IM,\mathbf{D},\mathbb{M}_{k}\right.\right)^{2}\right]$$

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Robust Fragility Assessment

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RF is defined as the expected value for a prescribed fragility model considering the joint probability distribution for the fragility model parameters $\boldsymbol{\theta}_k$. The RF herein can be expressed as:



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Recalling the Flowchart:



(URF





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Fragility curves for Chemical Industry Infrastructure Damaged due to 2011 Great East Japan earthquake and tsunami

Chua, C. T., Switzer, A. D., Suppasri, A., Li, L., Pakoksung, K., Lallemant, D., ... & Winspear, N. (2021). Tsunami damage to ports: cataloguing damage to create fragility functions from the 2011 Tohoku event. Natural Hazards and Earth System Sciences, 21(6) 1887-1908.




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European Tsunami Risk Service (ETRiS) - Data products from past tsunami events



Vulnerability curve based on data for the Chilean Tsunami 2010.

Mas, E., Koshimura, S., Suppasri, A., Matsuoka, M., Matsuyama, M., Yoshii, T., Jimenez, C., Yamazaki, F. and Imamura, F., 2012. Developing Tsunami fragility curves using remote sensing and survey data of the 2010 Chilean Tsunami in Dichato. *Natural Hazards and Earth System Sciences*, *12*(8), pp.2689-2697.

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Useful references and documentation

- Jalayer, Fatemeh, Hossein Ebrahimian, Konstantinos Trevlopoulos, and Brendon Bradley. "Empirical tsunami fragility modelling for hierarchical damage levels." *Natural Hazards and Earth System Sciences* 23, no. 2 (2023): 909-931.
- Behrens, Jörn, Finn Løvholt, Fatemeh Jalayer, Stefano Lorito, Mario A. Salgado-Gálvez, Mathilde Sørensen, Stephane Abadie et al.
 "Probabilistic tsunami hazard and risk analysis: A review of research gaps." *Frontiers in Earth Science* 9 (2021): 628772.
- The European Tsunami Risk Service: https://eurotsunamirisk.org/
- EPOS ICS-C Portal: https://www.ics-c.epos-eu.org/

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Some useful ETRiS Repositories

• Repository of fragility functions:

https://github.com/eurotsunamirisk/etris_data_and_data_products/tree/m

ain/etris_data_products/Fragility_Curves

Repository of Vulnerability Functions

https://github.com/eurotsunamirisk/etris_data_and_data_products/tree/m

ain/etris_data_products/Vulnerability_Curves

• ComputeFrag Software

https://eurotsunamirisk.org/tsunamirisktoolkit/

• Map Viewer

https://eurotsunamirisk.org/maps/

• Jupyter Notebooks for Fragility Visualisation

https://github.com/eurotsunamirisk/VisualizeFragility







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